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(57) Abstract

In CDMA systems (1) with time-variant multipath transmission channels, such as mobile radio systems, receivers are used that apply multipath diversity techniques so as to counteract fading. In a known CDMA system, L-tap RAKE receivers (20) are used of which taps are adjusted on the basis of channel estimation means (61) that estimates multipath delays (τ_{11}, ..., τ_{1L}; τ_{N1}, ..., τ_{NL}) from the received signal (y), i.e. searchers are arranged for finding paths. In such a system inter-user and inter-path interference is not taken into account. As a result, it is difficult to detect yet unresolved paths. Especially, it is difficult or even impossible to detect weak users in a strong user environment. A CDMA system (1) is proposed comprising channel estimation means (64) having a channel model for estimating ($\hat{y}$) the received signal (y). An interference reduced signal (e) is formed from the received signal (y) and the estimated received signal ($\hat{y}$) and is applied to the searchers. In an embodiment the channel model is an adaptive linear combiner (70 ... 80) combining re-spread decision feedback signals (b) weighted by estimated complex amplitudes (A) of resolved paths. Because in the interference reduced signal strong users are no longer present, it is easier to find yet unresolved paths. From the interference reduced signal (e) weak users can be easily detected, thus increasing system capacity.

"A multiple access digital transmission system and a radio base station and a receiver for use in such a system"

The present invention relates to a multiple access digital transmission system comprising at least one transmitter for transmitting at least one modulated datastream, and at least one receiver for receiving a transmitted signal, which comprises the modulated datastreams, via a transmission channel, the receiver comprising receiving means having

5   resolving means for resolving at least one path for at least one multipath received modulated datastream, and having channel estimation means, which are coupled to the resolving means, for estimating channel path delays in the received modulated datastreams. Such a transmission system can be a mobile radio multiple access system based upon direct-sequence spread spectrum techniques or the like, or other transmission systems using similar

10   techniques.
         The present invention further relates to a radio base station and to a receiver for use in such a system.

15   Spread spectrum systems are well-known since long and have been described in numerous articles and handbooks, such as in a basic article describing a system implementing a direct-sequence spread spectrum system, "A Communication Technique for Multipath Channels", R. Price et al., Proc. of the IRE Vol. 46, March 1958, pp. 555-570, a tutorial article "Theory of Spread-Spectrum Communications - A Tutorial", R. L. Pickholtz

20   et al, IEEE Tr. on Comm., Vol. COM-30, No. 5, May 1982, pp. 855-884, and a handbook "Digital Communications", J. Proakis, McGraw-Hill, 1989, Chapters 7 and 8. In Chapter 7, pp. 702-799 of said handbook digital signalling over fading multipath channels is described as is the case in a mobile radio system, in Chapter 7, pp. 719-739 a so-called RAKE receiver is described implementing diversity for multipath spread spectrum receivers, and in Chapter

25   8 spread-spectrum receivers, especially pp. 802-804, describing direct-sequence spread spectrum, pp. 831-836 describing PN sequences for DS SS, pp. 862-864, describing a sync acquisition phase for DS SS, and pp. 868-872, describing sync tracking for DS SS. In this respect it is to be noticed that synchronisation of a DS SS receiver to a DS SS transmitter has to be very accurate, i.e. within a fraction of a so-called chip in the tracking phase. In

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practical systems, the acquisition and tracking phases may not be quite distinguishable.

From the US-Patent No. 5,099,493 a DS-SS (Direct Sequence-Spread

Spectrum) Receiver is known with separate integrated signal estimator-and-demodulator

arrangements for processing DS-SS channels. A common error signal is formed as the

5   difference between the received signal and the sum of reconstructed signals estimated by the

estimator-and-demodulator units. Each reconstructed signal is also fed back to the input of

the corresponding estimator-and-demodulator unit. This approach does not exploit efficiently

the fact that the channel parameters vary slowly as compared to the bit period. Due to the

immediate feedback the channel estimates are sub-optimal. Furthermore, the US-Patent No.

10   5,099,493 is not directed to multipath signal path resolving, and the shown analog COSTAS-

loops are not particularly suitable for digital receivers.

A multiple access digital transmission system of the above kind is known

from the European Patent No. 0 361 299. In said patent a multiple access direct-sequence

spread spectrum system or CDMA (Code Division Multiple Access) mobile radio system is

15   disclosed. In such a mobile radio system the transmission channel between mobile radio

station and a base station, having a multipath behaviour, is apt to give fadings due to the fact

that such a multipath behaviour is time variant. I.e., signals arriving at the base station via

various paths of different phase shifts and different length and thus giving rise to different

path delays may cancel each other almost completely. In order to counter such situations, the

20   system disclosed in said patent applies wide band signals and channel estimation for

estimating channel path delays of a number of strong paths or rays per user. More generally,

in a multipath broad band channel systems in some form frequency selective fading occurs.

In a small band system such frequency selective fading would present itself as so-called flat

fading as a result of which total signal suppression could occur, a so-called deep fading.

25   Such a deep fading could, to some extent, be counter-acted by applying coding and

interleaving, but, better, by increasing the signal bandwidth whereby such flat fading is

perceived as frequency selective fading. Then, paths in the multipath channel can be resolved

by path delay estimation. The estimated path delays are applied to a so-called L-tap RAKE

demodulator as disclosed in figure 8, blocks 15 and 19 of said patent. The channel estimation

30   of the path delays is carried out in blocks 15, 17 and 18 of said figure 8. In said patent, for

finding L paths, N parallel correlators are applied, and N time shifted versions or replica of

the same generated pseudo-noise reference sequence used for despreading, L and N being

integers. In case N has a very large value, the correlator bank behaves like a so-called

matched filter. In said patent, the tasks of demodulation, path delay estimation, and

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amplitude estimation as the case may be, are solved by averaging techniques only, i.e. by applying correlators with a sufficiently large correlation gain. On the one hand, the correlation length may not be too small, because of an acceptable suppression of inter-user and inter-path interference, i.e. interference between users or between rays of the same user,

5 has to be achieved, and on the other hand, the correlation length may not be too long because of the fact that, in case of a mobile radio channel for instance, the mobile radio channel is time variant. The system according to said patent, though suppressing inter-user and inter-path interference to an acceptable extent, does not take into account inter-user interference, i.e. rays of other users causing interference with rays of the current user.

10 Resolved paths with different delays also cause noise-like interferences with demodulation. All in all, a situation can occur in which weak users cannot be detected. This problem is aggravated in mobile radio systems where the so-called near-far problem might arise, i.e. given that near and far users transmit with equal power, the signal from the near user will arrive at the receiver in question with a much larger power than that of the far user. This

15 might form so severe a problem that DS CDMA cannot be used, at least not without very sophisticated power control.

It is an object of the present invention to provide a multiple access digital

20 access system of the above kind which takes into account both inter-path and inter-user interference.

It is to this end the multiple access digital transmission system according to the present invention is characterized in that the receiving means comprises generating means for generating an interference reduced signal from the received signal, the interference

25 reduced signal being fed to the channel estimation means. Using the interference reduced signal allows to estimate the channel parameters more accurately. The present invention is based upon the insight that a delay in channel estimation is allowable if the channel parameters vary slowly with respect to the bit period. Such a delay can easily be implemented in a digital system. Inter-user interference is taken into account due to the fact

30 that the interference reduced signal virtually only contains components due to rays (and users, which, in a given case correspond to a datastream) that not have been taken into account. Since the interference in the interference reduced signal due to resolved rays is drastically reduced, not yet resolved weak or new rays can easily be detected. As compared with the prior art in which on the average strongest rays can be detected only, the present

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invention detects the currently strongest rays. Because a much smaller processing gain will do, the computational complexity of the present invention as compared to the prior art is reduced. Due to the reduced interference the total correlation length can be reduced. This implies that channel delays can be tracked more closely. When applied in a base station of a

5   mobile radio station, it implies improved access because of the fact that acquisition of a user and its path delays occurs faster and more accurate.

In an embodiment of the present invention, the receiving means comprises received signal estimation means for estimating the received signal, and subtracting means for subtracting the estimated signal from the received signal so as to form the interference

10   reduced signal, generation of the interference reduced signal being channel model based. In this way, with an explicit channel model, a very simple and accurate interference reduction is achieved.

In an embodiment of the present invention an amplitude and a phase per resolved path is estimated, the estimated amplitudes and phases being fed to the received

15   signal estimation means. It is achieved that resolved paths can be updated dynamically, current strongest paths being demodulated, and weaker resolved paths being deleted. Due to the achieved interference reduction, the amplitudes and phases can be determined very accurately.

In an embodiment of the present invention the amplitude and the phase is

20   recursively estimated. This implies a simple method giving an accurate estimation, and thus a good estimation of the received signal. Also, a good amplitude and phase estimation can be used with demodulation, thus improving the same.

In an embodiment of the present invention at least two receiving means are cascaded, an input of a succeeding receiving means being coupled to an interference

25   reduced signal output of a preceding receiving means, so as to successively detect stronger and weaker received modulated datastreams. Thus, also weak users can be detected with less demand on power control. This is based on the insight that weak users do not appear in the channel model of the preceding receiving means and do hardly contribute to interference, but on the other hand come to the fore in the succeeding receiving means because in the

30   interference reduced signal of the preceding receiving means the strong users are eliminated only. This also implies that weak users which cannot be detected by prior art systems can be detected in the system according to the present invention, thus leading to an increased system capacity.

In an embodiment of the present invention at transmission side, after

spreading, an inverse Fourier transform is applied, and at reception side, before despreading, a Fourier transform is applied. Thus, by combining CDMA with OFDM (orthogonal frequency division multiplexing) an extra degree of freedom in the system according to the present invention is achieved, because, with OFDM, the frequency range can be controlled.

5   I.e., chips in the frequency domain are obtained, which can be distributed over the frequency domain as is favourable for the transmission. At receiver side, the multipath channel is equalized in the frequency domain, then.

10   The present invention will now be described, by way of example, with reference to the accompanying drawings, wherein

         Fig. 1 schematically shows a CDMA mobile radio system according to the present invention,

         Fig. 2 shows an L-tap RAKE demodulator,

15   Fig. 3 shows a RAKE-finger for a RAKE demodulator,

         Fig. 4 shows a searcher for estimating path delays,

         Fig. 5 shows a first embodiment of a CDMA receiver according to the present invention,

         Fig. 6 shows an adaptive linear combiner according to the present

20   invention for use in a CDMA receiver,

         Fig. 7 shows a state-space multi-user detector as an alternative for the bank of RAKE demodulators,

         Fig. 8 shows a transmitter for use with a second embodiment of a CDMA receiver according to the present invention,

25   Fig. 9 shows a second embodiment of a CDMA receiver according to the present invention, and

         Fig. 10 shows a third embodiment of a CDMA receiver according to the present invention.

         Throughout the figures the same reference numerals are used for the same features.

30   features. Throughout the description complex variables are given bold-faced.

         Fig. 1 schematically shows a cellular CDMA (Code Division Multiple Access) mobile radio system 1 according to the present invention, comprising a number of

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base stations BS1 and BS2 covering respective radio zones Z1 and Z2. Each radio zone services a number of mobile radio stations MS1, MS2 and MS3, and MS4, MS5, and MS6, respectively. The radio base stations BS1 and BS2 are coupled to a mobile switching centre MSC via landlines 11 and 12. The mobile switching centre is coupled to the public telephone

5   switching network PSTN. The radio base stations are arranged for processing spread spectrum signals transmitted by the mobiles, i.e for processing uplink spread spectrum signals. Also the mobiles can be arranged to process spread spectrum signals from the base stations, i.e. can process downlink spread spectrum signals. Also hybrid systems are possible, e.g. FDMA (frequency division multiple access) transmission in the downlink

10   direction and CDMA transmission in the uplink direction. The radio base stations can even be arranged for processing signals from FDMA operating mobiles and CDMA operating mobiles, or for processing other combinations of signals. In the sequel, operating in CDMA mode according to the present invention will be described. A CDMA radio system is a multiple access system operating according to spread spectrum techniques, i.e. after coding

15   and/or interleaving of datastreams, as the case may be, these datastreams are frequency spread before transmission. At a reception side a received signal is despread, and de-interleaved and/or decoded, as the case may be. The datastreams may originate from a single user such as a mobile radio user, or may be combined datastreams originating from several users. In the given example, DS SS (direct sequence spread spectrum) is applied, whereby a

20   pseudo-random noise sequence is applied to a datastream, e.g. in case of a BPSK (binary phase shift keying) modulated binary datastream, the BPSK modulated datastream and the pseudo-noise sequence are applied to a modulo-two adder, at an output of which a spread datastream occurs. Despreading at receiver side is then achieved by applying the same pseudo noise sequence, which must thus be known in the receiver, to the received signal.

25   The present invention is not limited to BPSK, but other modulation method may be used. For a more detailed description of DS SS, referred is to chapter 8 of said handbook of Proakis. Such a CDMA mobile radio system operates in a multipath environment, i.e. radio signals from a mobile radio station to a radio base station, or vice versa, arrive at the radio base station via a multitude of paths, indicated in Fig. 1 with paths or rays p1 and p2.

30   Furthermore, the radio channel is time-variant. This may result in fadings at the receiver side, due to different phase shifts and path delays of multipath rays and addition thereof at receiver side. According to the present inventions the negative effects of both inter-path and inter-user interference to the detection of a transmitted datastream are at least mitigated. In Fig. 1 the mobile radio station MS6 is shown in more detail as far as the transmitting side is

concerned. Data dta to be transmitted are supplied to an encoder 2, e.g. forming (n, k) block
codes, i.e. k information bits at a time generate a code of length n. This code is fed to a
quadrature spread spectrum modulator so as to obtain a QPSK spread spectrum signal for
transmission. The modulator comprises a pseudo-noise sequence generator 3, followed by a
5   modulo-2 adder 4 and a balanced modulator 5 in one branch, and a pseudo-noise generator 6,
a modulo-2 adder 7 and a balanced modulator 8 in another branch. Data are transmitted at a
rate $1/T_b$, T_b being the bit period. At an output of the modulo-2 adders 4 and 7 so-called
chips occur, a chip being a pulse in the pseudo-noise sequence having a smallest period T_c.
E.g. a spreading factor of 42 complex chips per bit or 84 chips in the I and Q channel
10   together can be used. With a coded bit rate of 24 kbit/s (e.g. speech) this corresponds to a
chip rate of 1.008 Mchips/s. Output signals of the balanced modulators 5 and 8, which are
also coupled to respective 90° shifted cos and sine outputs of a carrier oscillator 9, are added
with an adder 10 and pulse-shaped with a filter 11 before transmission to the base station
BS2 via an antenna 12.
15   Fig. 2 shows an L-tap RAKE demodulator 20 for a receiver in a mobile
station or a radio base station as shown in Fig. 1, for demodulating a received multipath
spread-spectrum signal representing a transmitted datastream, e.g. originating from a single
user. The RAKE demodulator 20 comprises L so-called RAKE-fingers 21 and 22, L being an
integer, for demodulating a spread-spectrum signal received from a particular mobile radio
20   station, e.g. MS6, via L different paths. Each RAKE-finger provides a preliminary decision
variable of a single path. Output signals of the RAKE-fingers 21, 22 are added with an adder
22A so as to form a combined decision variable, which is supplied to a decoder (not shown)
for decoding and/or de-interleaving as the case may be. A received quadrature modulated
signal r(t) is fed to a known receiver front-end 23 in which it is sampled inter alia with a
25   sample clock having e.g. twice the chip rate so as to form a complex signal y comprising all
direct and multipath signals of all received mobiles. The signal y forms an input signal for
all RAKE-fingers in the RAKE demodulator 20, for a single mobile. In case the
demodulation is carried out in a radio base station, it comprises N parallel RAKE
demodulators for demodulating N channels, N being an integer. Each RAKE-finger has an
30   input for a pseudo-noise signal PN and an input for a delay adjustment signal D_1, ..., D_L,
respectively. A vector $D = (D_1, ..., D_L)$ denotes a set of L tap delays. For a more detailed
description of a RAKE demodulator referred is also to said article of Price. Further shown in
Fig. 2 are a channel 24 for the mobile radio station MS6, a received signal of which adds
with signals received from other mobiles, e.g. MS4 and MS5, indicated with an addition

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symbol 25. The received signal r(t) further comprises additive assumed noise N_0, indicated
with an addition symbol 26.

Fig. 3 shows a RAKE-finger, e.g. the finger 21, for the RAKE
demodulator 20. The finger 21 comprises a variable delay buffer 31 to which the complex

5   signal y is supplied. An output of the delay buffer 31 is fed to two quadrature despreading
branches for despreading an in-phase component of a transmitted signal and for despreading
a quadrature component of the transmitted signal. The delay buffer 31 delays the path signal
comprised in the signal y such that the total delay is constant for all fingers, i.e. with τ_i, i =
1, ..., L being the path delays of the L strongest paths, τ_i + D_i is constant for all i. The

10   delays D_i are referred to as tap delays of the RAKE demodulator 20. The in-phase branch
comprises a delay unit 32, which delays over half the chip period T_c, and a cross correlator
formed by a multiplier 33 and an integrate and dump unit 34. The delay unit 32 is added for
offset QPSK. With offset QPSK, the transmitter is less demanding. The complex path signal
is cross correlated with an in-phase pseudo-noise sequence PN_I, and a quadrature pseudo-

15   noise sequence PN_Q, which may originate from the same generator (not shown), whereby the
sequences have different initial states, or may originate from different generators (not
shown). The quadrature branch comprises a multiplier 36 for multiplying the complex path
signal by -j, j $= \sqrt{-1}$, followed by a cross correlator formed by a multiplier 37 and an
integrate and dump unit 38. Outputs of the dump units 34 and 38 are added with an adder 39

20   of which an output is fed to a multiplier 40. A signal A_1^* is supplied to an input of the
multiplier 40, the signal A_1^* being a conjugate of a complex amplitude estimate A_1 of the
current path, as estimated according to the present invention. The multiplier 40 is followed
by a real-part-forming unit 41 which provides the preliminary decision variable. By
supplying estimates of complex amplitudes of the time-varying impulse response to the

25   RAKE demodulator 20, coherent detection is achieved. Supplying accurately estimated
complex amplitudes to the RAKE-demodulator, as according to the present invention,
achieves an improved performance of the RAKE demodulator 20.

Fig. 4 shows a searcher for estimating path delays which determines the
path delays and herewith the delays D from a short term delay power spectrum of the

30   channel. For N channels to be searched, a bank of N parallel searchers of this kind is
provided. The searchers continuously scan the range of possible delays and decide on the
presence of a ray. The searchers are correlators that use the spreading sequences together
with previous bit decisions in order to provide a correlation gain which is sufficiently large
for detection. According to the present invention, the searchers are provided with an error

signal e, being the difference between the signal y and an estimate of y. It will be described in the sequel how the error signal or interference reduced signal e is obtained. An embodiment of the searcher will be given. Other suitable searchers will also do, e.g. the searcher as to the cited European patent No. 0 361 299, Fig. 8, blocks 15, 17, and 18

5   thereof. The searcher comprises constant delay units 50 and 51 to which the in-phase and quadrature sequences PN_I and PN_Q are fed, respectively. The interference reduced signal e is matched filtered with re-modulated and re-spread previous bit decisions $\hat{b}_1$, acquired from decision feedback. The order of the matched filter determines the time window for which the delay power spectrum is estimated. A coefficient vector for matched filtering is updated after

10 each measurement interval, and the delay power spectrum is determined via averaging of several measured impulse responses after squared absolute values are taken. To this end the searcher further comprises units 52 and 53 for setting filter coefficients, time-variant matched filters 54 and 55, a unit 56 for taking squared absolute values, a filter 57 for averaging several short term delay power spectra, if necessary, and a path selection unit 58 for

15 selecting paths from the acquired averaged delay power spectrum.

        Fig. 5 shows a first embodiment of a CDMA receiver 60 according to the present invention. The receiver front end, comprising a channel filter and sampling means inter alia, is not shown in detail. Receiving means 60 for one channel is shown in detail. For indicating that there are N detectors in parallel for N channels to be demodulated, the

20 demodulators not shown in detail are shown in a quasi three-dimensional way of displaying. Block 64 is common to all channels. Channel estimation means 61 for estimating path delays for a multipath channel are provided as described in relation to Fig. 4. The RAKE demodulator 20 for resolving the paths are provided as described in relating to Fig. 2. The receiver further comprises a pseudo-noise generator 62 for providing a pseudo-noise

25 sequence PN_1 corresponding to the pseudo-noise sequence of channel one applied at transmitter side, a decision feedback unit 63 for providing a previous bit decision $\hat{b}_1$, and received signal estimation means 64 according to the present invention for generating an estimate $\hat{y}(k-k_0)$ of the received signal $y(k)$ and the interference reduced signal $e(k-k_0)$ to be fed to the searcher 61, k denoting the sampling period. A delay unit 65 is provided for

30 delaying the received signal y by k_0, corresponding to a predetermined number of samples. This is due to the decision feedback used, necessary for determining an estimate $\hat{y}$ for y. The delay k_0 is determined by the maximum time required for demodulation which is basically the maximum bit period plus the maximum delay spread of the channel. Further shown is an adder 66 for obtaining the signal e. According to the present invention at least to a great

extent all interference is cancelled simultaneously. For detecting weak users, similar multi-user receivers may be connected in series, indicated with the dashed blocks 68 and 69 connected in series. According to the present invention, the error signal e does not comprise strong rays anymore. Thus, weak users can easily be detected from the error signal e. In the

5   given embodiment all processing is done by an ASIC (Application Specific Integrated Circuit) or by a DSP (Digital Signal Processor) or by a number of DSPs comprising ROM (Read Only Memory) and RAM (Random Access Memory). Such a DSP, well-known in the art per se, is not further shown in detail. Further, a decoder 67 is shown, which provides decoded data, e.g. speech data.

10   Fig. 6 shows an ALC (Adaptive Linear Combiner) as the received signal estimation means 64 according to the present invention for use in a CDMA receiver. The ALC 64 comprises re-spread and modulation means 70 and 71 for re-spreading the decision feedback bits b_1 and b_N so as to obtain the signals $v_1(k)$ and $v_N(k)$ which are fed to delay units 72 and 73, and 74 and 75, respectively, representative of path delays τ_{11}, ..., τ_{1L}, and path

15   delays τ_{N1}, ..., τ_{NL}, for L strongest paths for each of N channels. The signals $v_n(k)$, when superimposed, would give the received sampled signal y(k) when assuming no multipath fading. To include multipath fading, the signals v are delayed with the path delays τ and weighted and phase shifted on the basis of the estimated complex amplitudes A_{nl}, $n = 1, ..., N$, and $l = 1, ..., L$, before addition by means of a combiner 76 so as to form

20   the signal $\hat{y}$. In Fig. 6, further shown are complex multipliers 77, 78, 79, and 80, and a complex adder 81. The path delays are continuously acquired by the searchers as described in relation to Fig. 4. Newly estimated path are offered to the ALC 64. The ALC 64 determines whether to interchange paths or to disregard the new paths. Thus, the ALC 64 always chooses the strongest paths. For simplifying notation the computational feedback k_0 is

25   assumed zero, i.e. in the sequel k is used instead of $k-k_0$. The ALC reflects a common baseband multi-user channel model, modelling L strongest rays for each of N users. The complex amplitudes A_{nl} of the ALC 64 are updated jointly using an LMS (Least Mean Square) algorithm. This is a very practical choice as to implementation because it is a low complexity algorithm and exchanging, adding or removing of rays or users is very simple.

30   The estimate $\hat{y}$ and the complex amplitudes A_{nl} are updated according to:

$$\hat{y}(k) = \sum \sum A_{nl}(k).v_n(k-\tau_{nl}), \text{ whereby}$$

summation is over $n = 1, ..., N$ and $l = 1, ..., L$,

inverse Fourier transform means 118. As before, also channel estimation means for estimating path delays 119, and a channel model 120 is provided. In this embodiment the multipath channel is equalized in the frequency domain. As in the first embodiment, the channel model operates in the time domain.

5   Fig. 10 shows a third embodiment of a CDMA receiver according to the present invention. This receiver is a modification of the receiver shown in Fig. 9. A serial-to-parallel converter 200, and Fourier transform means 201 are provided, common to the N channels. Furthermore, the receiver comprises an ALC 202, operating in the frequency domain, Fourier transform means 203 for Fourier transforming outputs of the ALC 202, so 10   as to form the interference reduced signal e via parallel-to-serial converter means 204. When embodying the channel estimation means 61 for estimating path delays in the frequency domain, the Fourier transform means 203 and the parallel-to-serial converter means 204 can be dispensed with. Such an embodiment is useful when the users are synchronized with respect to each other, i.e. FFT-blocks of different users should be received synchronously, 15   then.

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and, $A_{nl}(k+1) = A_{nl}(k) + \mu.v_n^*(k-\tau_{nl}).e(k),$

for n = 1, ..., N, and l = 1, ..., L. The symbol * denotes a complex conjugate operation. In the above formulas, μ is an adaptation step size of the LMS algorithm. In an embodiment, the LMS algorithm is run on the sampling rate. According to the present invention the

5   complex amplitudes are estimated more accurately as compared to simplest correlation and averaging techniques, because interference is taken into account during a joint adaptation process. As a result, performance of the RAKE demodulators is increased.

Fig. 7 shows a state-space multi-user detector as an alternative for the bank of RAKE demodulators. The state space detector comprises means 90 for estimating a

10   state vector, and a unit 91 comprising a channel model including re-spreading and modulation. A Kalman estimation error $e_{KA}(k)$ is inputted to the estimator 90. Inputs of the re-spreading unit 91 are the pseudo-noise sequences PN_1, ..., PN_N, and estimated channel parameters cp for N users, as described before. An output of the estimator is the signal $\hat{b}(k)$ comprising all transmitter bits of all N users influencing the received signal y(k) at time k.

15   For a more detailed description of a state-space multi-user detector, referred is to the article "A State-Space Multiuser Detector for CDMA Systems", J. Thielecke, IEEE Int. Conf. on Comm., ICC 1993, Vol. 3, pp. 1762-1767. Also, a state-space multi-user detector is disclosed in the PCT Application WO 94/00116, filed by the same applicant on 20 May 1994, the contents of this application herewith being incorporated by reference.

20   Fig. 8 shows a transmitter 100 for use with a second embodiment of a CDMA receiver according to the present invention, comprising a spreading unit 101 as described in relation to Fig. 1, spreading the data dta with M chips per bit, M being an integer, and further comprising inverse Fourier transform means 102 acting upon the spread data, parallel-to-series conversion means 103 for obtaining a serial data stream from the

25   inverse Fourier transformed chips, and transmit means 104 including a transmit filter. In such a transmitter 100, CDMA is combined with OFDM. In this case chips are obtained in the frequency domain. These chips, or bins in the frequency domain, can be distributed over the frequency domain such that a favourable transmission is achieved.

Fig. 9 shows a second embodiment of a CDMA receiver according to the

30   present invention, comprising a receiver front end 110, sampling means 111, a serial-to-parallel converter 112, Fourier transform means 113, an equalizer 114, and despreading means 115, for N channels. Outputs of the despreading means are fed to a decoder, and to decision feedback means 116, as before. Decision feedback variables are re-spread, as before, and fed, after serial-to-parallel conversion in a serial-to-parallel converter 117, to

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CLAIMS:

1.   A multiple access digital transmission system (1) comprising at least one transmitter (MS6) for transmitting at least one modulated datastream (dta), and at least one receiver (BS2) for receiving (y) a transmitted signal, which comprises the modulated datastreams, via a multipath transmission channel, the receiver comprising receiving means

5   (60) having resolving means (20) for resolving at least one path for at least one multipath received modulated datastream, and having channel estimation means (61), which are coupled to the resolving means (20), for estimating channel path delays $(\tau_{11}, ..., \tau_{1L}; \tau_{N1}, ..., \tau_{NL})$ in the received modulated datastreams, characterized in that the receiving means (60) comprises generating means (64, 65, 66) for generating an interference reduced signal (e) from the

10   received signal (y), the interference reduced signal (e) being fed to the channel estimation means (61).

2.   A multiple access digital transmission system (1) according to claim 1, wherein the receiving means (60) comprises received signal estimation means (70 ... 80) for estimating ($\hat{y}$) the received signal (y), and subtraction means (66) for subtracting the

15   estimated signal ($\hat{y}$) from the received signal (y) so as to form the interference reduced signal (e), generation of the interference reduced signal being channel model based.

3.   A multiple access digital transmission system according to claim 2, wherein an amplitude and a phase (A) per resolved path is estimated, the estimated amplitudes and phases being fed to the received signal estimation means (70 ... 80).

20   4.   A multiple access digital transmission system (1) according to claim 3, the amplitude and the phase is recursively estimated.

5.   A multiple access digital transmission system according to claims 2, 3, or 4, wherein the received signal estimation means (70 ... 80) is an adaptive linear combiner.

6.   A multiple access digital transmission system according to claims 1, 2, 3,

25   4 or 5, wherein the resolving means (20) is a RAKE demodulator.

7.   A multiple access digital transmission system according to claims 1, 2, 3, 4 or 5, wherein the resolving means is a joint multi-user detector (90, 91).

8.   A multiple access digital transmission system according to any one of the preceding claims, wherein at least two receiving means (60, 68, 69) are cascaded, an input

of a succeeding receiving means being coupled to an interference reduced signal output of a preceding receiving, so as to successively detect stronger and weaker received modulated datastream.

9.   A multiple access digital transmission system according to claim 1, wherein at transmission side, after spreading, an inverse Fourier transform (102) is applied, and at reception side, before despreading, a Fourier transform (113) is applied.

10.   A radio base station for use in a multiple access digital transmission system, the radio base station comprising a receiver for receiving a signal, which comprises modulated datastreams, transmitted via a transmission channel, the receiver comprising receiving means having resolving means for resolving at least one path for at least one multipath received modulated datastream, and having first channel estimation means, which are coupled to the resolving means, for estimating channel path delays in the received modulated datastreams, characterized in that the receiving means (60) comprises generating means (64, 65, 66) for generating an interference reduced signal (e) from the received signal (y), the interference reduced signal (e) being fed to the channel estimation means (61).
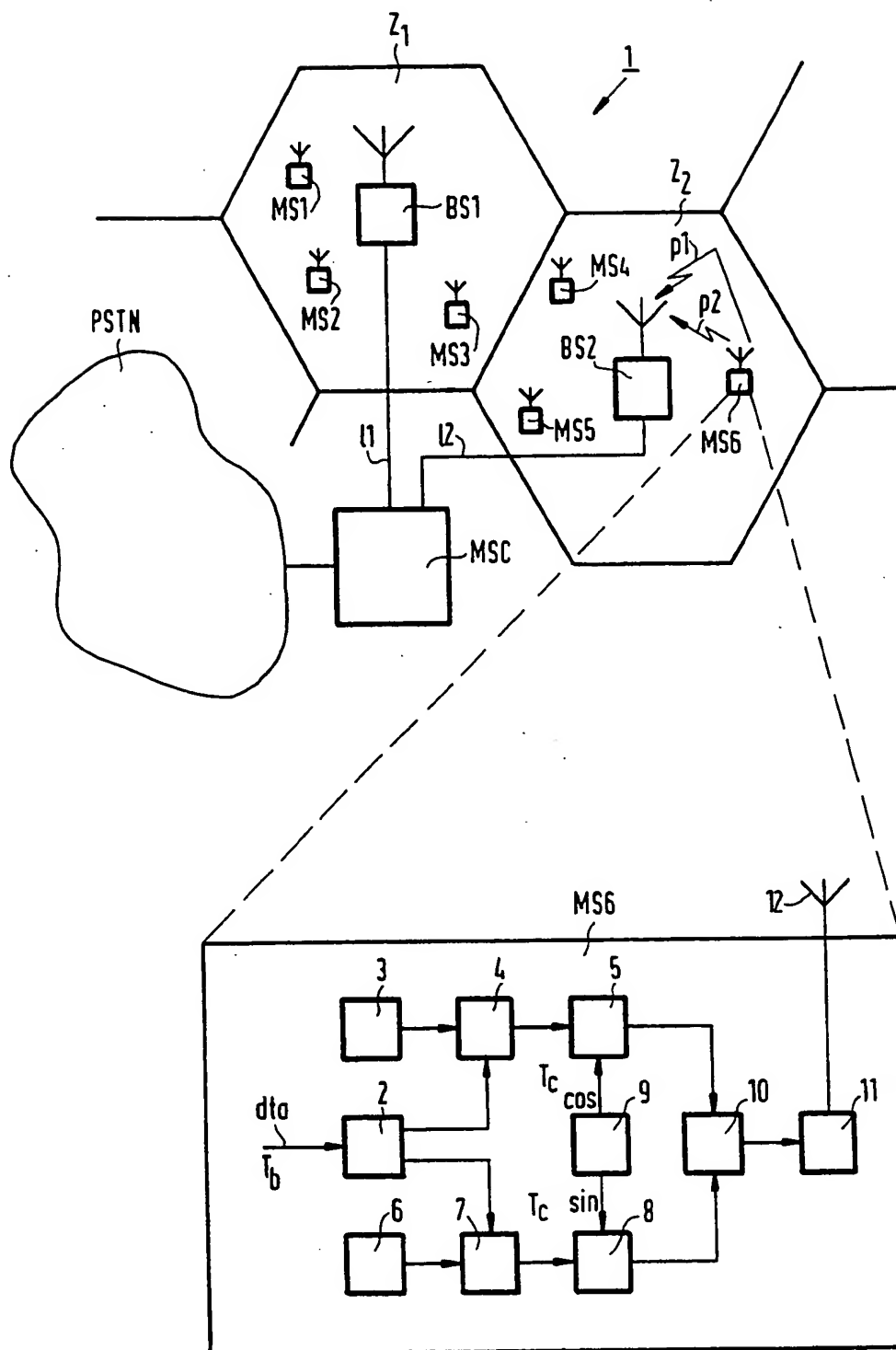
11.   A receiver for use in a multiple access digital transmission system, the receiver comprising receiving means for receiving a signal, which comprises modulated datastreams, transmitted via a multipath transmission channel, the receiving means having resolving means for resolving at least one path for at least one multipath received modulated datastream, and having first channel estimation means, which are coupled to the resolving means, for estimating channel path delays in the received modulated datastreams, characterized in that the receiving means (60) comprises generating means (64, 65, 66) for generating an interference reduced signal (e) from the received signal (y), the interference reduced signal (e) being fed to the channel estimation means (61).
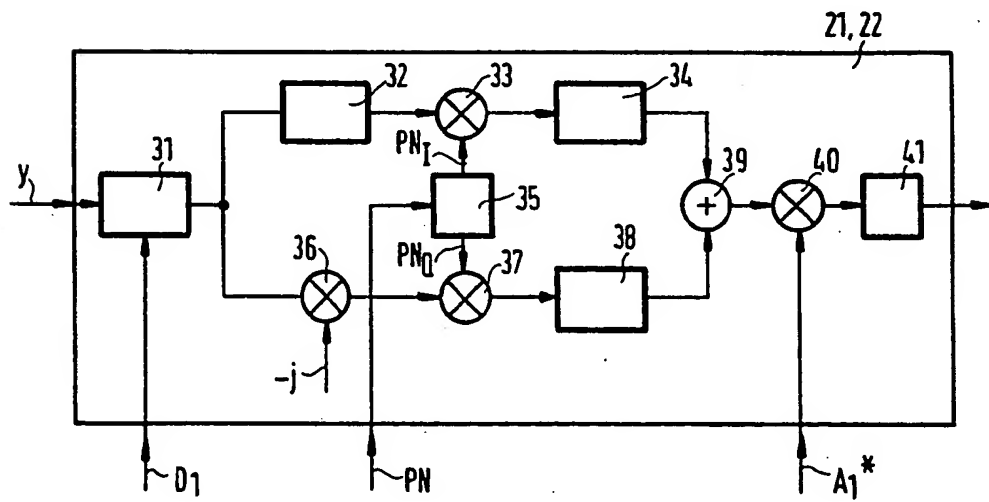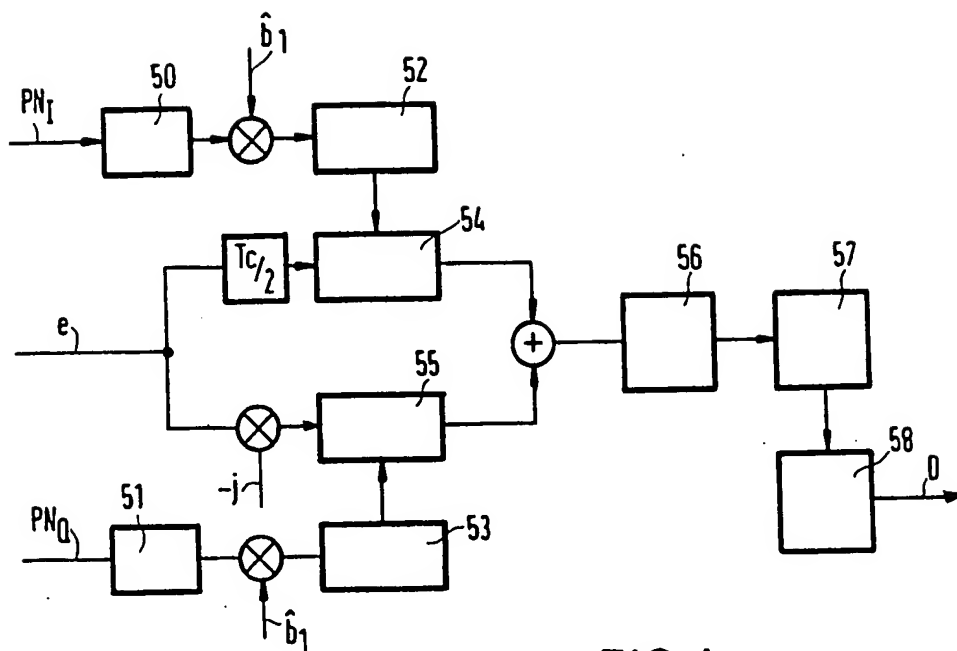
FIG.1

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FIG. 2

FIG. 3

FIG.4
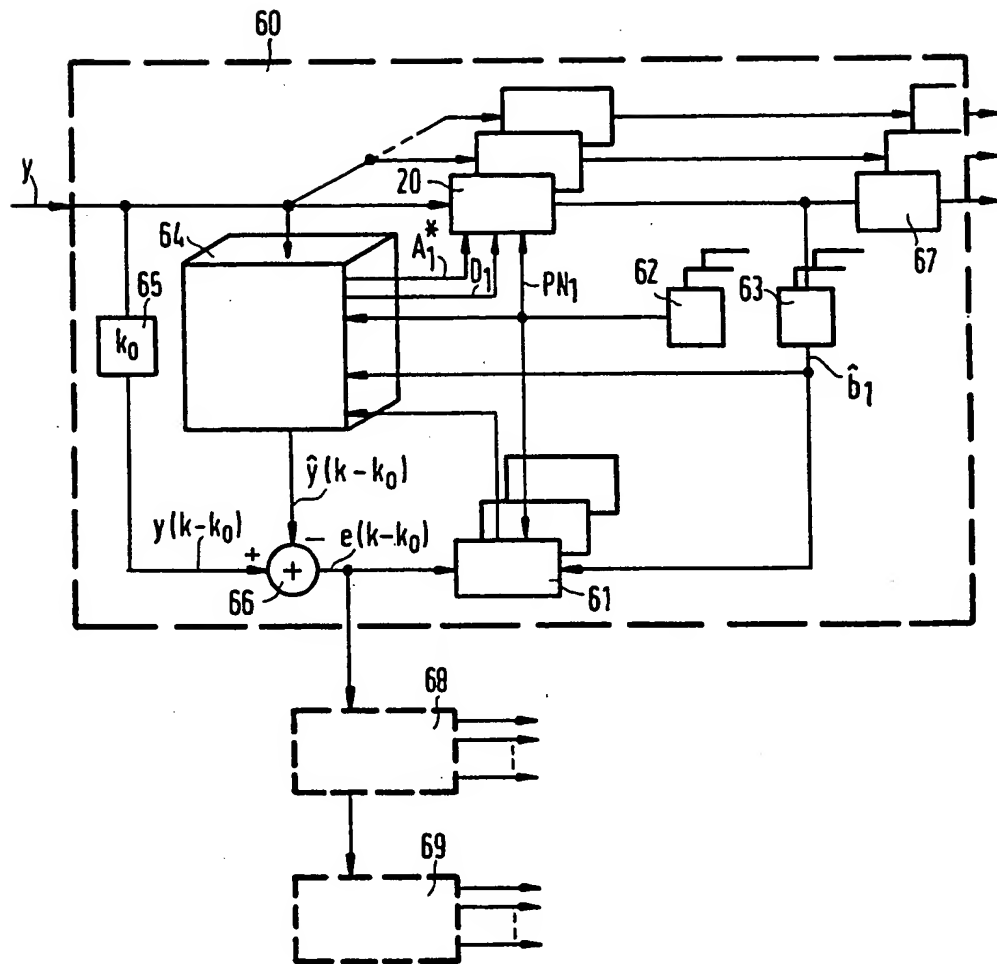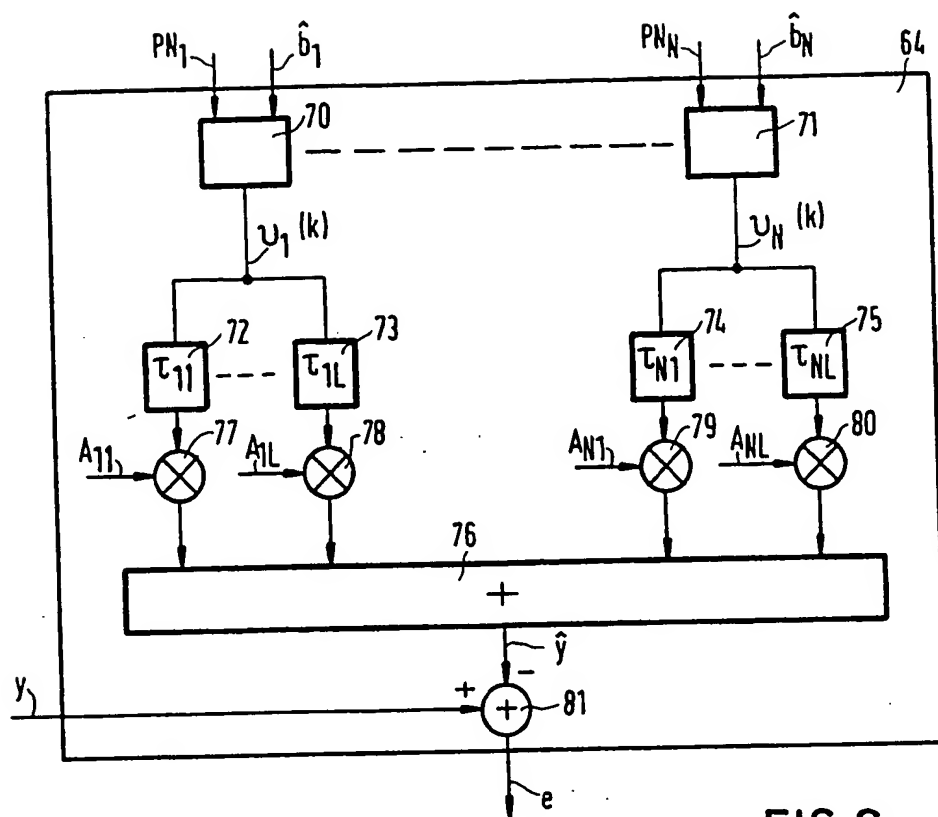

FIG.7

FIG.5

FIG.6

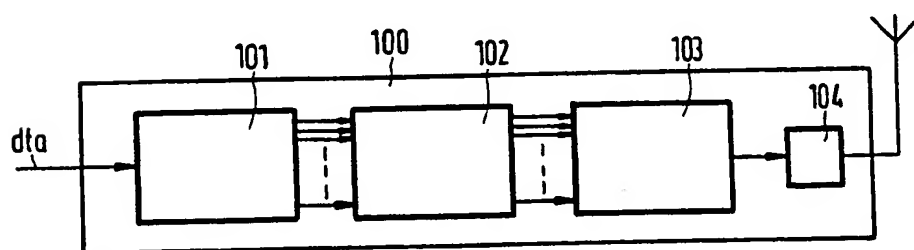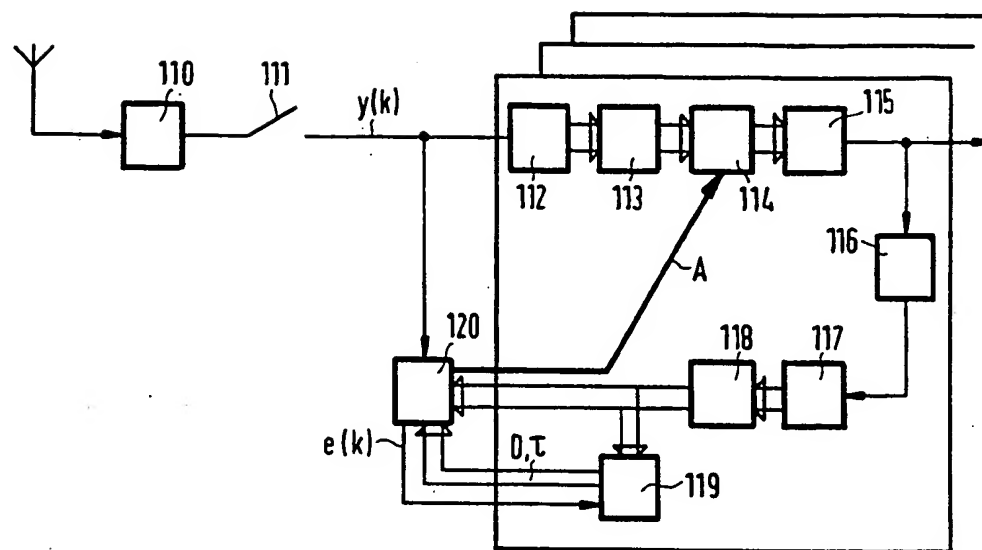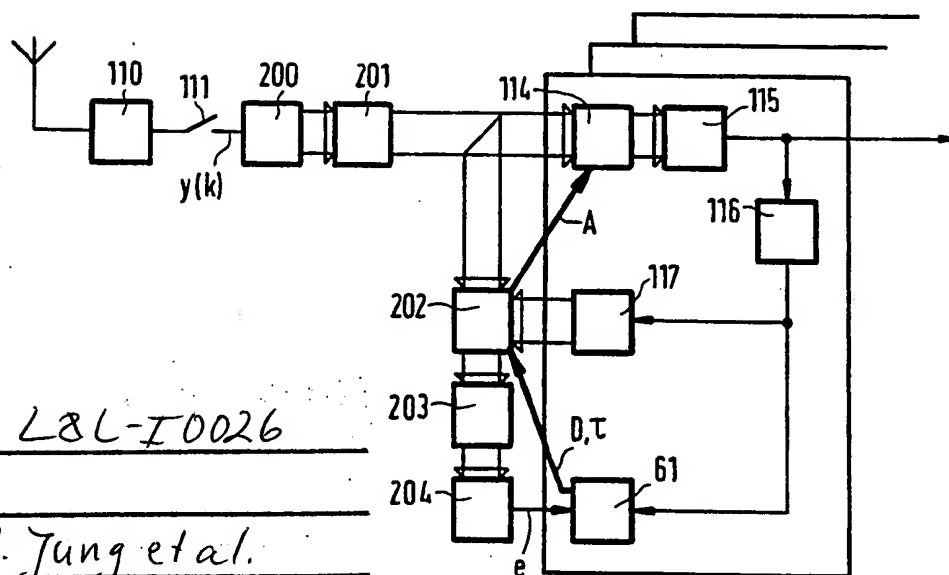FIG.8

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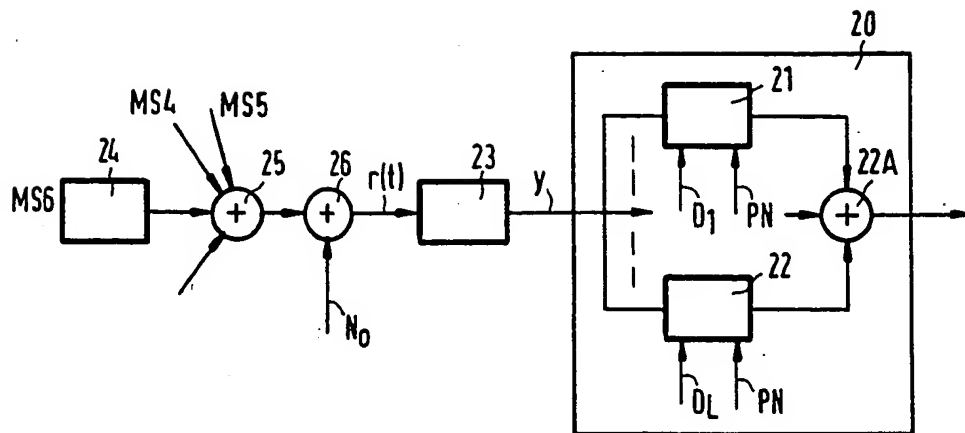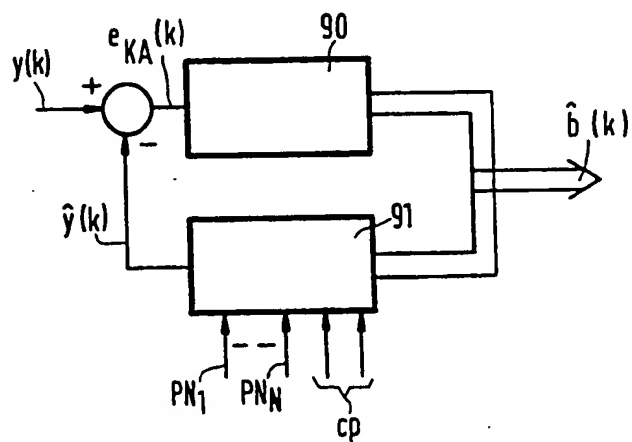
FIG.9

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FIG.10